



NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

INTERACTIVE COMPUTER PROGRAM
FOR THE
ANALYSIS AND DESIGN OF LINEAR
TIME INVARIANT SYSTEMS

by

Habib Ismail

December 1984

Thesis Advisor:

G. J. Thaler

Approved for public release; distribution is unlimited.

T222120

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Interactive Computer Program for the Analysis and Design of Linear Time Invariant Systems		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis; December 1984
7. AUTHOR(s) Habib Ismail		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93943		12. REPORT DATE December 1984
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		13. NUMBER OF PAGES 62
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution is unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Interactive Program, Bode Plot, Linear Control Systems		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) In this thesis, an interactive computer program for the analysis and design of time invariant unity feedback control systems is presented, using cascade or feedback or both types of compensation. By using this program, the user is freed from the tedious, time consuming and error prone method of hand calculations, letting the computer handle these tasks		

efficiently and speedily. The user can then concentrate fully on the placement of poles and zeroes of the compensator(s) used.

Design of control systems by classical methods being essentially a repetitive, trial and error procedure, this program greatly cuts down the turn around time and leads to faster, more satisfactory results.

Approved for public release; distribution is unlimited.

Interactive Computer Program
for the
Analysis and Design of Linear Time Invariant Systems

by

Habib Ismail
Lieutenant Commander, Pakistan Navy
B.E., University of Karachi, Pakistan, 1974

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL
December 1984

ABSTRACT

In this thesis, an interactive computer program for the analysis and design of time invariant unity feedback control systems is presented, using cascade or feedback or both types of compensation.

By using this program, the user is freed from the tedious, time consuming and error prone method of hand calculations, letting the computer handle these tasks efficiently and speedily. The user can then concentrate fully on the placement of poles and zeroes of the compensator(s) used.

Design of control systems by classical methods being essentially a repetitive, trial and error procedure, this program greatly cuts down the turn around time and leads to faster, more satisfactory results.

DRAFT
10/10/68
MONTEREY, CALI
OL
13943

TABLE OF CONTENTS

I.	INTRODUCTION	9
II.	CONTROL ENGINEERING ANALYSIS	11
	A. GENERAL	11
	B. PROBLEM FORMULATION	12
	C. COMPUTER AIDED DESIGN	14
III.	PROGRAMMING CONSIDERATIONS	16
	A. GENERAL	16
	B. MAIN FEATURES OF THE PROGRAM	16
	C. PROGRAM DESCRIPTION	18
IV.	PROGRAM PERFORMANCE INVESTIGATION	20
	A. GENERAL	20
	B. EXAMPLE PROBLEMS	20
	1. Example 4.1 : A Phase Lead Network	20
	2. Example 4.2 : A Lag/Lead Network	26
	3. Example 4.3 : Velocity Feedback	31
V.	CONCLUSION AND RECOMMENDATIONS	37
	A. CONCLUSION	37
	B. RECOMMENDATIONS	38
	1. Curve Fitting	38
	2. Computer Selection of Compensators	38

3.	Root Locus	39
4.	Integrated Control System Design	39
APPENDIX PROGRAM LISTING		40
LIST OF REFERENCES		60
INITIAL DISTRIBUTION LIST		61

LIST OF TABLES

1.	Tabular Output of Example 4.1	24
2.	Tabular Output of Example 4.2	29
3.	Tabular Output of Example 4.3	34

LIST OF FIGURES

1.	Types of Compensators	13
2.	Uncompensated Bode Plot of Example 4.1	22
3.	Lead Compensation Bode Plot of Example 4.1	23
4.	Uncompensated Bode Plot for Example 4.2	27
5.	Lag/Lead Compensation of Example 4.2	28
6.	Uncompensated Bode Plot of Example 4.3	32
7.	Velocity Feedback Used in Example 4.3	33
8.	Closed Loop Response of Example 4.3	36

I. INTRODUCTION

During the past two decades, the scientific and engineering communities have witnessed an ever increasing role of the digital computer in the fields of research, development and analysis of systems. The computer, today, is being used to solve engineering problems, whose solution, until very recently required long and tedious procedures. Still, it is probably true that this machine has potential not fully recognized yet, which is why the attention of so many computer scientists/engineers is focused on devising more efficient and innovative operating procedures.

Control system design is one area where classical theory has been extensively developed and used. It is fair to say that even today, most analysis and design problems of linear, time invariant control systems can still be approached using the methods developed by Bode, Nyquist and others.

A totally new approach to the design of control systems became available with the development of optimal control theory and the state variable analysis. These methods have been intensively developed in the last 10-15 years, but now their weaknesses have been exposed too. The "states" of the plant may not necessarily represent physically measurable quantities, and consequently it may not be possible to

implement the results at all. Luenberger's observers, designed to overcome this problem, can at best provide estimates of the state trajectory. Furthermore, the optimal control approach to design relies very heavily on mathematical manipulation, providing little insight to the actual working of the plant; the only input of the designer being the form of the cost function.

An intelligent use of the speed and information processing ability of the digital computer, coupled with the reliable features of classical theory appear to be the best solution to the problem at hand. The classical approach to design, being essentially a trial and error method, if the order of the system is fairly high, the number of repetitive calculations and the time required to perform these calculations becomes prohibitively large, the assistance of the computer in such problems becomes indispensable.

The work in this thesis was to develop an interactive, user oriented computer program that would prompt the user to input the transfer function and cascade/feedback compensators. The program would then display on the IBM 3277 - Tektronix 618 dial screen terminals the Bode Plot of both magnitude and phase. The program could be repeatedly used, with the user having the option to change/modify the compensators, each time viewing the effect of his modifications on the screen until he arrives at a satisfactory solution.

II. CONTROL ENGINEERING ANALYSIS

A. GENERAL

A continuous time control system may be represented in one of the following forms:

- a. Transfer functions
- b. State equations
- c. System block diagrams or signal flow graphs

Algorithms exist in almost every undergraduate control engineering text to convert the system representation from one given form to another. Gianniotis (Ref. 1) describes a simple method of converting from transfer function to state variable form in Chapter II.

The transfer function representation in its most general form is:

$$\frac{A_m s^m + A_{m-1} s^{m-1} + A_{m-2} s^{m-2} + \dots + A_0 s^0}{B_n s^n + B_{n-1} s^{n-1} + B_{n-2} s^{n-2} + \dots + B_0 s^0}$$

Usually the mathematical description of the system is found in the transfer function form in the literature. Analysis and design of control systems by classical methods also requires the representation of the system in this form.

This thesis does not address the problem of converting from one form of representation to another. It is assumed that any conversions necessary have already been performed and that the system is represented by its open loop transfer function.

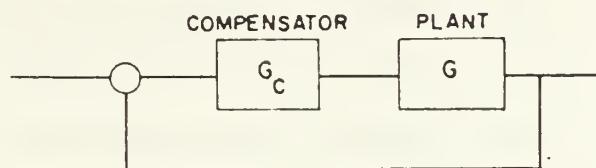
B. PROBLEM FORMULATION

Each system design has its own unique characteristics, but in general the system has to meet some kind of performance standards. These performance standards are generally provided as numerical specifications. The first step in the design of a control system is to analyze the system by itself in the usual feedback loop configuration. This is usually referred to as the uncompensated system.

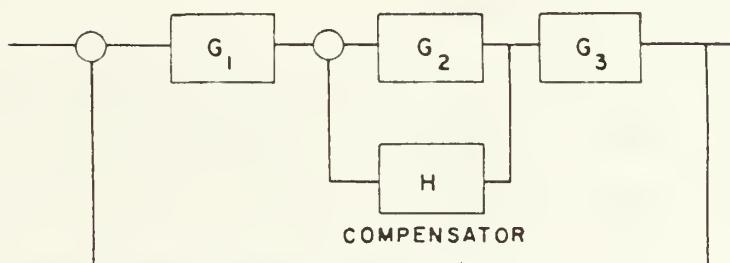
Analysis of the uncompensated system almost always shows that the system cannot meet some or all of the given performance standards. Usually, additional components have to be inserted in the system for the purpose of altering the performance of the system. These components are called compensators. Compensation is a two step procedure, in which additional components (compensators) are inserted to change the structure of the system, and these components are then adjusted until the performance characteristics are satisfied.

The theory of cascade and feedback compensation is discussed in detail by Thaler (Ref. 2) in Chapters 5 and 6. Only a brief discussion of the types of compensators is presented here.

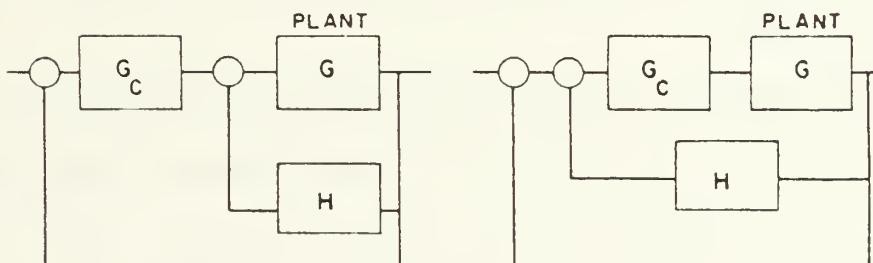
Compensators used in the design of feedback control systems are generally classified as shown in the block diagrams of figure 1.



a) CASCADING COMPENSATION



b) FEEDBACK COMPENSATION



c) COMBINED CASCADING AND FEEDBACK COMPENSATION

Figure 1. Classification of Compensation Structures

Cascade compensation may further be classified into two further types; a high pass filter usually called a phase lead compensator, and a low pass or phase lag compensator.

The selection of the type of compensator(s) to be used depends on a number of factors, the important ones being experience, personal preferences, availability, system constraints, etc. Unfortunately, there are no mathematical techniques to help in this selection process. Generally, one has to complete several designs and then choose the most appropriate one.

C. COMPUTER AIDED DESIGN

Of all the classical design methods available, the Bode diagram technique is generally considered to be the simplest, at the same time providing the most insight into system performance and behavior. The Bode design method may be used equally effectively both with cascade and feedback compensation schemes.

The computer program developed in this thesis displays on the terminal, initially, the Bode diagram (magnitude and phase) of the uncompensated open loop system. The user may then select the type of compensator to be used, and feed this information to the computer. The display changes, now showing the compensated system Bode Plot. This procedure may be repeated iteratively, with the computer updating the Bode Plot with each change made.

It was found on the average that turn around time for a typical third order system with two cascade compensators is less than five minutes.

III. PROGRAMMING CONSIDERATIONS

A. GENERAL

Any interactive software package, such as the one developed in this thesis must provide a simple yet unambiguous means of data input and output. The data must be easy to interpret and apply to the problem at hand. Programs producing highly satisfactory results but requiring long studying time and/or special programming skills are of limited use only.

The intent of this thesis is to present such a program, Computer Aided Design of Linear Systems. Special care has been taken to develop the program so that the user has to invest very little time learning to use it.

B. MAIN FEATURES OF THE PROGRAM

The development of a user oriented interactive computer program in solving engineering problems requires a considerable amount of programming work, contributing significantly to its complexity and size.

The computer program, hereafter referred to as BODPLT consists of a main program, a number of programmer-composed subroutines, a few library functions/subroutines, and various subroutines of the DISSPLA graphics package. The entire program is written in the FORTRAN IV language.

In brief, the whole BODPLT package works as follows:

A user, logged into the VM/CMS environment of the system from the dual screen terminals, issues the command DISSPLA BODPLT. The package then assumes control. The program begins its execution by interrogating the user and calling the appropriate subroutine accordingly. All programmer-composed subprograms are included in the main program titled BODPLT FORTRAN.

The BODPLT program has the following important features:

- runs of the VM/CMS time sharing system.
- interrogates the user in entering all problem specifications from the terminal.
- can handle up to a ninth order plant transfer function, six first order and one second order cascade filters.
- prompts the user to input the parameters of velocity feedback, acceleration feedback or approximate acceleration feedback as required.
- provides the solution in tabular form on the IBM 3277 screen and the Bode Plot on the TEK 618 terminal.
- can provide hard copy version of the problem specifications and tabular output by using the RECORD ON/RECORD OFF execs, and of the BODE PLOT on the Tektronix printer where installed.
- allows problem specifications to be changed between runs.

C. PROGRAM DESCRIPTION

The main program is the coordination center which controls the calling of the supporting subroutines, in order to input the transfer function, cascade/feedback compensators and other necessary information. The tabular results and the Bode Plot are then displayed on the two screens respectively.

The main program as well as the accompanying subroutines can be found in Appendix A. They contain a sufficient number of comment cards to be self explanatory.

The following is a brief description of the performance and purpose of the various subroutines.

NUMER inputs the numerator of the plant transfer function.

DENOM inputs the denominator of the plant transfer function.

CASCAD inputs up to 6 first order lead/lag filters.

SECAS inputs the numerator of the second order band pass/band stop filter.

SECASD inputs the denominator of the second order filter.

FETCH determines the value of the radial frequency, w , at the origin of the x-axis.

DECADE determines the number of decades of frequency to be spanned.

FEEDBK inputs the various parameters of feedback compensators.

TITLES inputs the two lines of text as headings for the Bode Plot.

In addition, the main program handles the tasks of displaying the tabular output and the Bode Plot of the open and closed loop response of the system as required.

IV. PROGRAM PERFORMANCE INVESTIGATION

A. GENERAL

The program was tested by solving several linear control system design problems. Very satisfactory results were obtained in all cases with remarkable efficiency and speed. The only necessary condition is proper problem formulation. This is true for any interactive computer program. Once the program is used a couple of times, the user gets the necessary familiarity with its working.

The example problems presented below are used to demonstrate the performance and capabilities of the program. The examples can also help the user in formulating his own particular problem. The examples were selected from Thaler's 'Design of Feedback Systems' (Ref. 2)

B. EXAMPLE PROBLEMS

1. Example 4.1 : A Phase Lead Network

a. Problem Statement

A positioning system is single loop with unity feedback and forward transfer function

$$G(s) = \frac{5.0}{s(0.7s + 1)(0.3s + 1)}$$

The velocity constant is not to be decreased. Design a phase lead compensator which will provide M_{pw} less than 1.5.

b. Solution

The first step is to get the transfer function in the required form:

$$G(s) = \frac{5.0}{0.21s^3 + 1.0s^2 + 1.0s} \quad (4.2)$$

The Bode Plot of the uncompensated system drawn using the program is shown on figure 2 and the tabular output on table 1. The uncompensated system has a phase margin of -20 degrees. To achieve a M_{pw} of less than 1.5, a phase margin of 44 degrees or more is required. Approximately 64 degrees of positive phase shift are therefore needed. Two sections of lead filter are introduced as given below:

$$G_c = \frac{(s/3.0 + 1)(s/1.5 + 1)}{(s/10.0 + 1)^2}$$

The compensated Bode Plot is given on figure 3 showing a phase margin of 35 degrees.

It may be pointed out that the final values for the lead filter poles and zeroes were arrived at after 3 iterations and this design problem was solved in less than 15 minutes.

EXAMPLE 4.1

UNCOMPENSATED SYSTEM

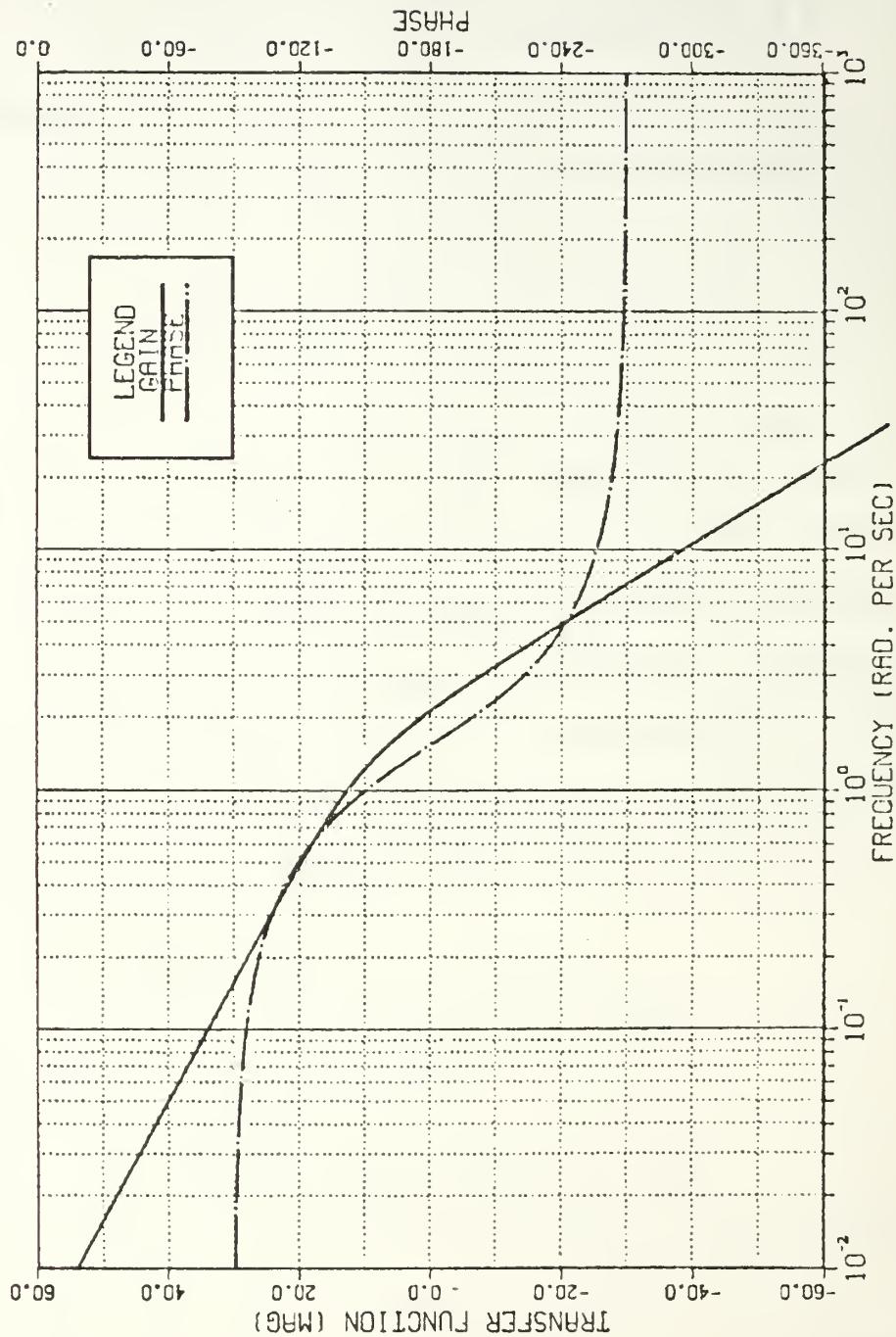


Figure 2. Uncompensated Bode Plot of Example 4.1

EXAMPLE 4.1
LEAD COMPENSATION

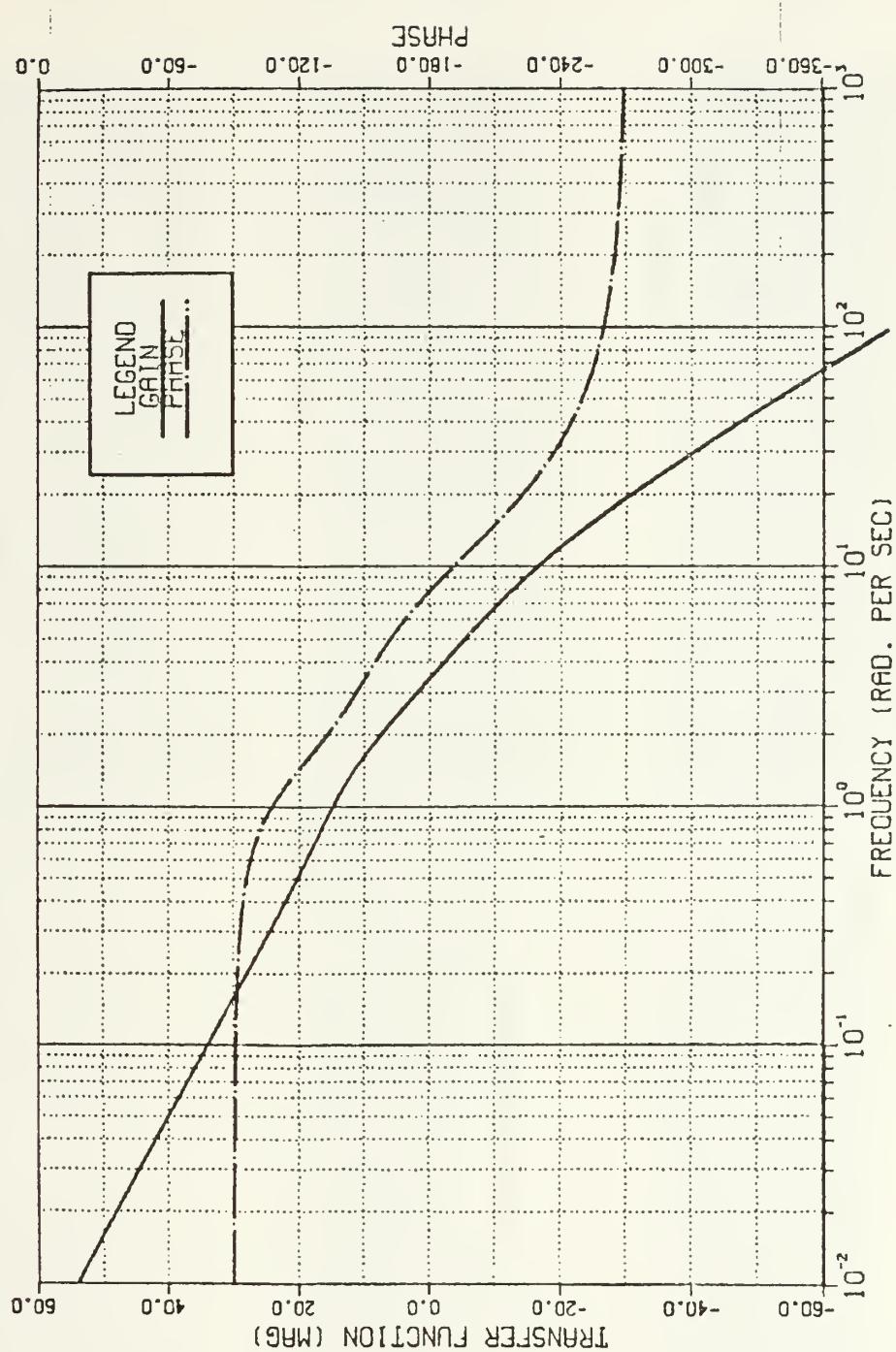


Figure 3. Lead Compensation Bode Plot of Example 4.1

Table 1. Tabular Output of Example 4.1

FREQ	MAGNITUDE	PHASE
0.100000E-01	0.539790E+02	-0.904134E+02
0.110776E-01	0.530907E+02	-0.901258E+02
0.122712E-01	0.522019E+02	-0.901395E+02
0.135936E-01	0.513130E+02	-0.901546E+02
0.150584E-01	0.504242E+02	-0.901714E+02
0.160810E-01	0.495354E+02	-0.901900E+02
0.184785E-01	0.486466E+02	-0.902106E+02
0.204697E-01	0.477579E+02	-0.902335E+02
0.226754E-01	0.468691E+02	-0.902588E+02
0.251188E-01	0.459804E+02	-0.902868E+02
0.278256E-01	0.450918E+02	-0.903179E+02
0.308240E-01	0.442032E+02	-0.903524E+02
0.341455E-01	0.433146E+02	-0.903905E+02
0.378249E-01	0.424262E+02	-0.904329E+02
0.419008E-01	0.415378E+02	-0.904798E+02
0.464158E-01	0.406490E+02	-0.905318E+02
0.514175E-01	0.397615E+02	-0.905890E+02
0.569580E-01	0.388736E+02	-0.906536E+02
0.630956E-01	0.379859E+02	-0.907247E+02
0.698946E-01	0.370985E+02	-0.908036E+02
0.774263E-01	0.362114E+02	-0.908913E+02
0.857695E-01	0.353247E+02	-0.909887E+02
0.950117E-01	0.344385E+02	-0.910972E+02
0.105250E+00	0.335529E+02	-0.912180E+02
0.116591E+00	0.326680E+02	-0.913520E+02
0.129155E+00	0.317841E+02	-0.915030E+02
0.143072E+00	0.309012E+02	-0.916711E+02
0.158489E+00	0.300196E+02	-0.918295E+02
0.175567E+00	0.291397E+02	-0.920711E+02
0.194480E+00	0.282617E+02	-0.923094E+02
0.215443E+00	0.273860E+02	-0.925787E+02
0.238658E+00	0.265130E+02	-0.928840E+02
0.264370E+00	0.256433E+02	-0.932318E+02
0.292864E+00	0.247775E+02	-0.936298E+02
0.324421E+00	0.239162E+02	-0.940870E+02
0.359381E+00	0.230600E+02	-0.946171E+02
0.398106E+00	0.222096E+02	-0.952343E+02
0.441004E+00	0.213655E+02	-0.959547E+02
0.488526E+00	0.205278E+02	-0.968035E+02
0.541168E+00	0.196960E+02	-0.978075E+02
0.599489E+00	0.188709E+02	-0.989995E+02
0.664081E+00	0.180487E+02	-0.100417E+03
0.735540E+00	0.172265E+02	-0.102103E+03
0.814911E+00	0.163984E+02	-0.104101E+03
0.902723E+00	0.155561E+02	-0.106450E+03
0.999999E+00	0.146882E+02	-0.109181E+03
0.110775E+01	0.137807E+02	-0.112300E+03
0.122712E+01	0.128181E+02	-0.115704E+03
0.135935E+01	0.117855E+02	-0.119567E+03
0.150583E+01	0.106723E+02	-0.123548E+03
0.166809E+01	0.947399E+01	-0.127000E+03
0.184785E+01	0.819452E+01	-0.131594E+03
0.204696E+01	0.684498E+01	-0.135427E+03
0.226754E+01	0.544122E+01	-0.139032E+03
0.251188E+01	0.399998E+01	-0.142404E+03
0.278255E+01	0.253684E+01	-0.145561E+03
0.308239E+01	0.106322E+01	-0.148567E+03
0.341454E+01	-0.413782E+00	-0.151495E+03
0.378247E+01	-0.189175E+01	-0.154429E+03
0.419007E+01	-0.337225E+01	-0.157444E+03

Table 1. (Contd.)

0.464157E+01	-0.480013E+01	-0.100608E+03
0.514174E+01	-0.636283E+01	-0.163974E+03
0.569579E+01	-0.78934E+01	-0.167576E+03
0.630955E+01	-0.944966E+01	-0.171432E+03
0.693945E+01	-0.110539E+02	-0.175540E+03
0.774261E+01	-0.127116E+02	-0.179883E+03
0.857692E+01	-0.144313E+02	-0.184433E+03
0.950116E+01	-0.162196E+02	-0.189133E+03
0.105250E+02	-0.180814E+02	-0.193930E+03
0.115591E+02	-0.200195E+02	-0.198782E+03
0.129155E+02	-0.220340E+02	-0.203012E+03
0.143072E+02	-0.241238E+02	-0.20809E+03
0.158489E+02	-0.262850E+02	-0.213003E+03
0.175567E+02	-0.285134E+02	-0.217469E+03
0.194485E+02	-0.308033E+02	-0.221735E+03
0.215443E+02	-0.331486E+02	-0.225776E+03
0.238658E+02	-0.355431E+02	-0.229574E+03
0.264375E+02	-0.379807E+02	-0.233121E+03
0.292863E+02	-0.404556E+02	-0.236416E+03
0.324421E+02	-0.429023E+02	-0.239402E+03
0.359380E+02	-0.454962E+02	-0.242267E+03
0.398106E+02	-0.480529E+02	-0.244840E+03
0.441004E+02	-0.506288E+02	-0.247195E+03
0.488526E+02	-0.532208E+02	-0.249344E+03
0.541167E+02	-0.558260E+02	-0.251302E+03
0.599483E+02	-0.584423E+02	-0.253083E+03
0.664080E+02	-0.610677E+02	-0.254700E+03
0.735639E+02	-0.637005E+02	-0.256168E+03
0.814910E+02	-0.663395E+02	-0.257498E+03
0.902722E+02	-0.689835E+02	-0.258703E+03
0.999998E+02	-0.716317E+02	-0.259793E+03

EXAMPLE 4.2
UNCOMPENSATED SYSTEM

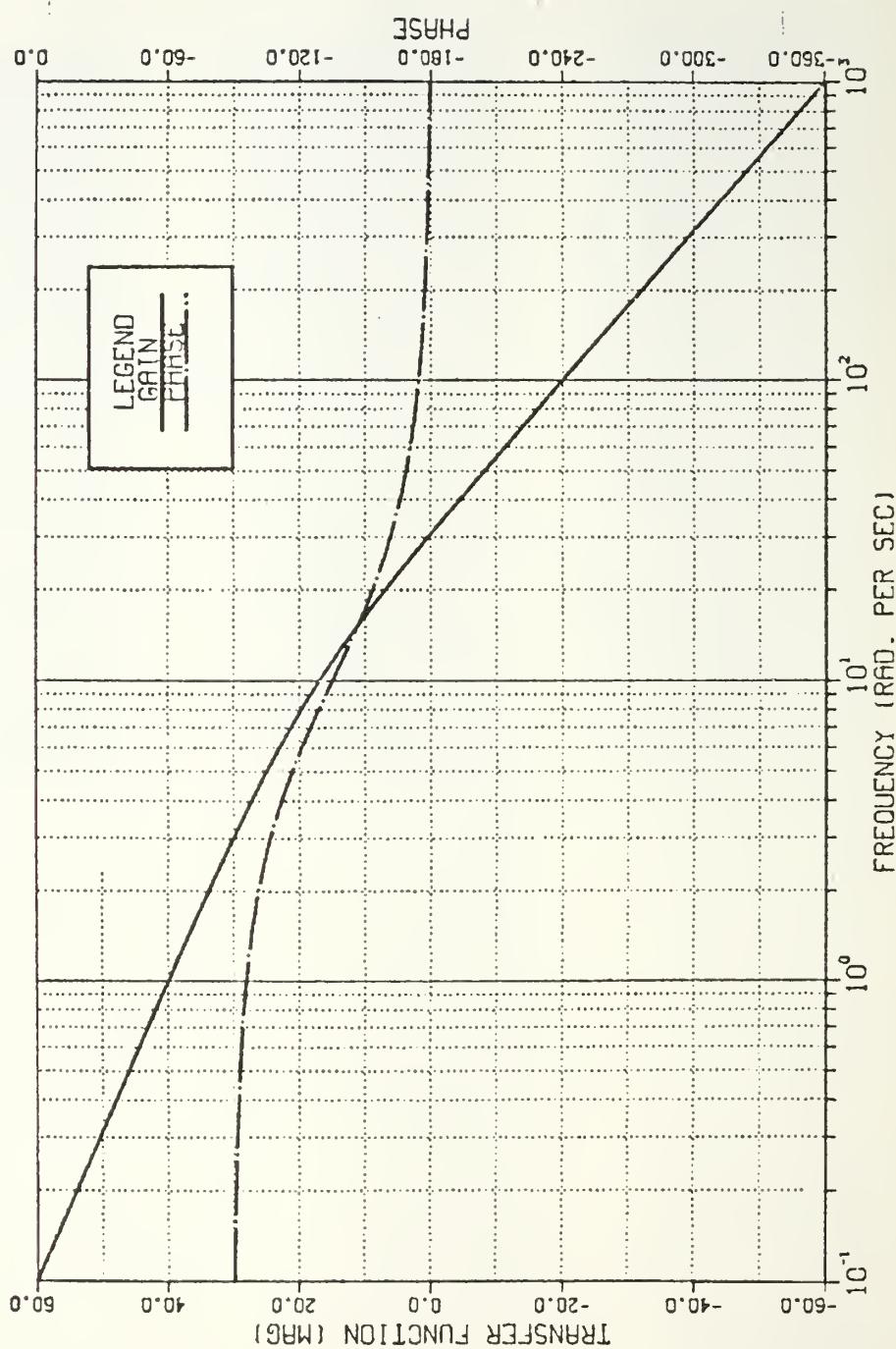


Figure 4. Uncompensated Bode Plot of Example 4.2

EXAMPLE 4.2
LAG/LEAD COMP.

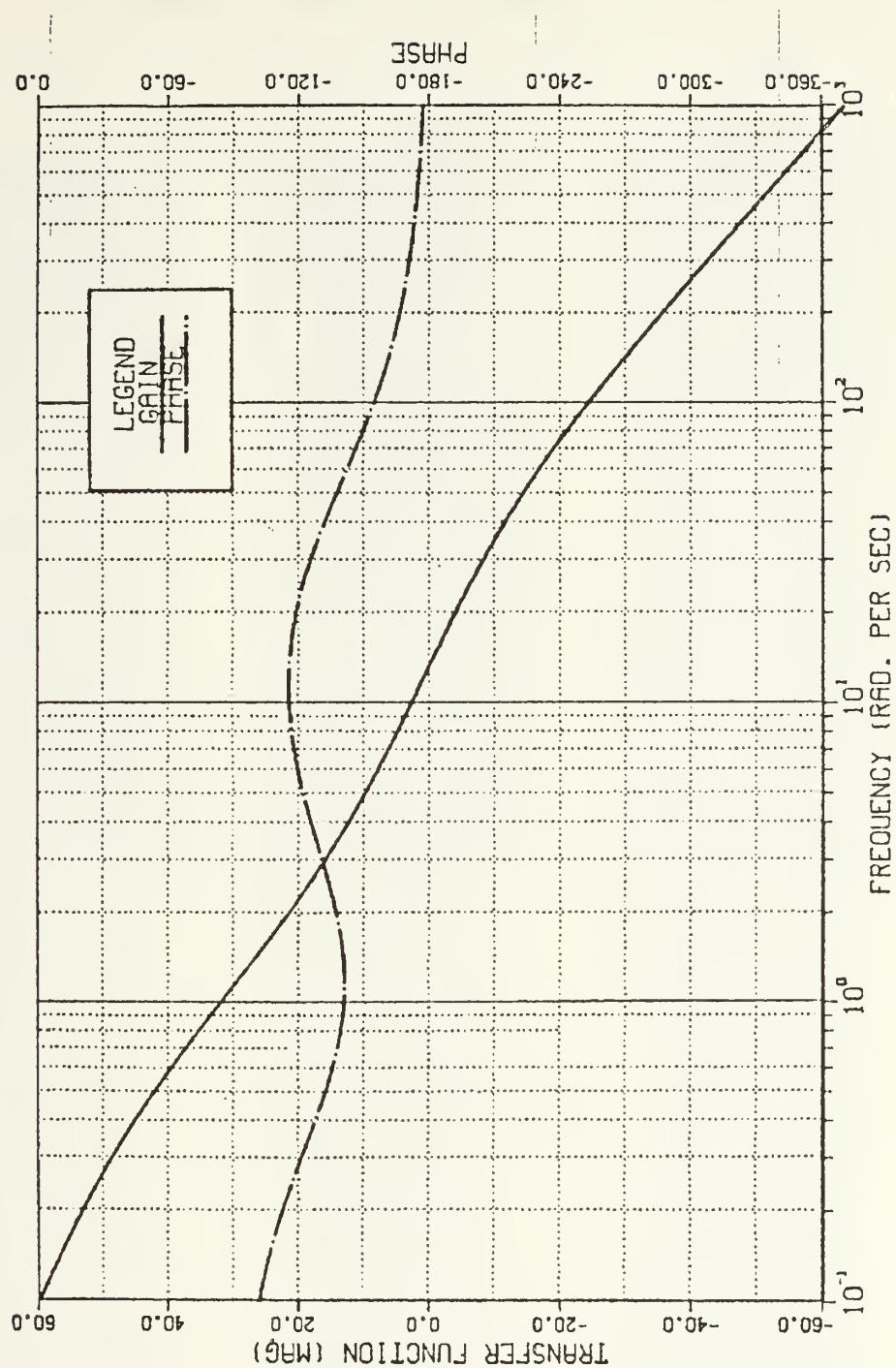


Figure 5. Lag/Lead Compensation in Example 4.2

Table 2. Tabular Output of Example 4.2

FREQ	MAGNITUDE	PHASE
0.100000E+00	0.598345E+02	-0.995141E+02
0.110776E+00	0.584089E+02	-0.100503E+03
0.122712E+00	0.579754E+02	-0.101580E+03
0.135935E+00	0.570325E+02	-0.102769E+03
0.150584E+00	0.560783E+02	-0.104058E+03
0.166810E+00	0.551106E+02	-0.105457E+03
0.184785E+00	0.541270E+02	-0.106908E+03
0.204697E+00	0.531249E+02	-0.108594E+03
0.226754E+00	0.521012E+02	-0.110334E+03
0.251188E+00	0.510529E+02	-0.112174E+03
0.278256E+00	0.499765E+02	-0.114115E+03
0.308240E+00	0.488887E+02	-0.116138E+03
0.341454E+00	0.477266E+02	-0.118226E+03
0.378248E+00	0.465474E+02	-0.120355E+03
0.419008E+00	0.453289E+02	-0.122491E+03
0.464158E+00	0.440698E+02	-0.124600E+03
0.514175E+00	0.427697E+02	-0.126603E+03
0.569580E+00	0.414292E+02	-0.128623E+03
0.630956E+00	0.400502E+02	-0.130449E+03
0.698946E+00	0.386350E+02	-0.132106E+03
0.774203E+00	0.371891E+02	-0.133500E+03
0.857695E+00	0.357155E+02	-0.134785E+03
0.950117E+00	0.342201E+02	-0.135758E+03
0.105250E+01	0.327090E+02	-0.130401E+03
0.116591E+01	0.311881E+02	-0.130884E+03
0.129155E+01	0.296640E+02	-0.137022E+03
0.143072E+01	0.281432E+02	-0.136877E+03
0.158489E+01	0.266320E+02	-0.136457E+03
0.175567E+01	0.251367E+02	-0.135773E+03
0.194485E+01	0.236031E+02	-0.148533E+03
0.215443E+01	0.222164E+02	-0.133710E+03
0.238658E+01	0.208014E+02	-0.132395E+03
0.264375E+01	0.194217E+02	-0.130927E+03
0.292864E+01	0.180801E+02	-0.129351E+03
0.324421E+01	0.167783E+02	-0.127709E+03
0.359381E+01	0.155106E+02	-0.126043E+03
0.398106E+01	0.142947E+02	-0.124393E+03
0.441004E+01	0.131107E+02	-0.122797E+03
0.480526E+01	0.119624E+02	-0.121289E+03
0.541168E+01	0.108466E+02	-0.119899E+03
0.599483E+01	0.975994E+01	-0.118052E+03
0.664081E+01	0.869860E+01	-0.117569E+03
0.735640E+01	0.765877E+01	-0.116066E+03
0.814911E+01	0.663658E+01	-0.115955E+03
0.902723E+01	0.562823E+01	-0.115445E+03
0.999999E+01	0.463006E+01	-0.115145E+03
0.110775E+02	0.363853E+01	-0.115060E+03
0.122712E+02	0.265011E+01	-0.115192E+03
0.135935E+02	0.166130E+01	-0.115547E+03
0.150583E+02	0.668658E+00	-0.115125E+03
0.166809E+02	-0.391396E+00	-0.116927E+03
0.184784E+02	-0.134252E+01	-0.117953E+03
0.204696E+02	-0.236847E+01	-0.119201E+03
0.226754E+02	-0.341315E+01	-0.120000E+03
0.251188E+02	-0.448058E+01	-0.122349E+03
0.278255E+02	-0.557484E+01	-0.12419E+03
0.308239E+02	-0.669992E+01	-0.126281E+03
0.341454E+02	-0.785960E+01	-0.128510E+03
0.378247E+02	-0.905738E+01	-0.130883E+03
0.419007E+02	-0.102961E+02	-0.133373E+03

Table 2. (Contd.)

0.464157E+02	-0.115780E+02	-0.135950E+03
0.514174E+02	-0.129043E+02	-0.138581E+03
0.569579E+02	-0.142753E+02	-0.141232E+03
0.630955E+02	-0.156905E+02	-0.143871E+03
0.698945E+02	-0.171484E+02	-0.148467E+03
0.774261E+02	-0.186460E+02	-0.148993E+03
0.857692E+02	-0.201824E+02	-0.151427E+03
0.950116E+02	-0.217522E+02	-0.153749E+03
0.105250E+03	-0.233528E+02	-0.155948E+03
0.115591E+03	-0.249806E+02	-0.158014E+03
0.129155E+03	-0.266322E+02	-0.159944E+03
0.143072E+03	-0.283043E+02	-0.161730E+03
0.158489E+03	-0.299941E+02	-0.163392E+03
0.175567E+03	-0.310988E+02	-0.164917E+03
0.194485E+03	-0.334161E+02	-0.166910E+03
0.215443E+03	-0.351439E+02	-0.167597E+03
0.238658E+03	-0.366805E+02	-0.168765E+03
0.264375E+03	-0.386245E+02	-0.169830E+03
0.292863E+03	-0.403745E+02	-0.170798E+03
0.324421E+03	-0.421296E+02	-0.171678E+03
0.359380E+03	-0.438888E+02	-0.172476E+03
0.398105E+03	-0.456513E+02	-0.173199E+03
0.441004E+03	-0.474166E+02	-0.173854E+03
0.488525E+03	-0.491842E+02	-0.174447E+03
0.541167E+03	-0.509536E+02	-0.174984E+03
0.599482E+03	-0.527247E+02	-0.175469E+03
0.664080E+03	-0.544969E+02	-0.175907E+03
0.735639E+03	-0.562702E+02	-0.176304E+03
0.814940E+03	-0.580443E+02	-0.176662E+03
0.902721E+03	-0.598190E+02	-0.176986E+03
0.999958E+03	-0.615944E+02	-0.177278E+03

3. Example 4.3 : Velocity Feedback

a. Problem Statement

A simple second-order servo is to be compensated with tachometer feedback. The forward transfer function is

$$G(S) = \frac{100.0}{S(S + 1)}$$

and the tachometer transfer function is $K_t S$. The tachometer is fed back around all of the forward gain. Using Bode diagram methods, set K_t to provide $M_{pw} = 1.3$.

b. Solution

Bode Plot for this system is shown on figure 6. The system has a phase margin of about 6 degrees. For $M_{pw} = 1.3$, a phase margin of 45 degrees is required. A rough graphical design on the uncompensated Bode Plot gives

$$1/H = 12.0/S \quad \text{or} \quad H = 0.08S$$

The Bode Plot for the compensated system is on figure 7, showing a phase margin of 50 degrees.

The close loop frequency response of this example, drawn using BODPLT is shown on figure 8.

EXAMPLE 4.3

UNCOMPENSATED SYSTEM

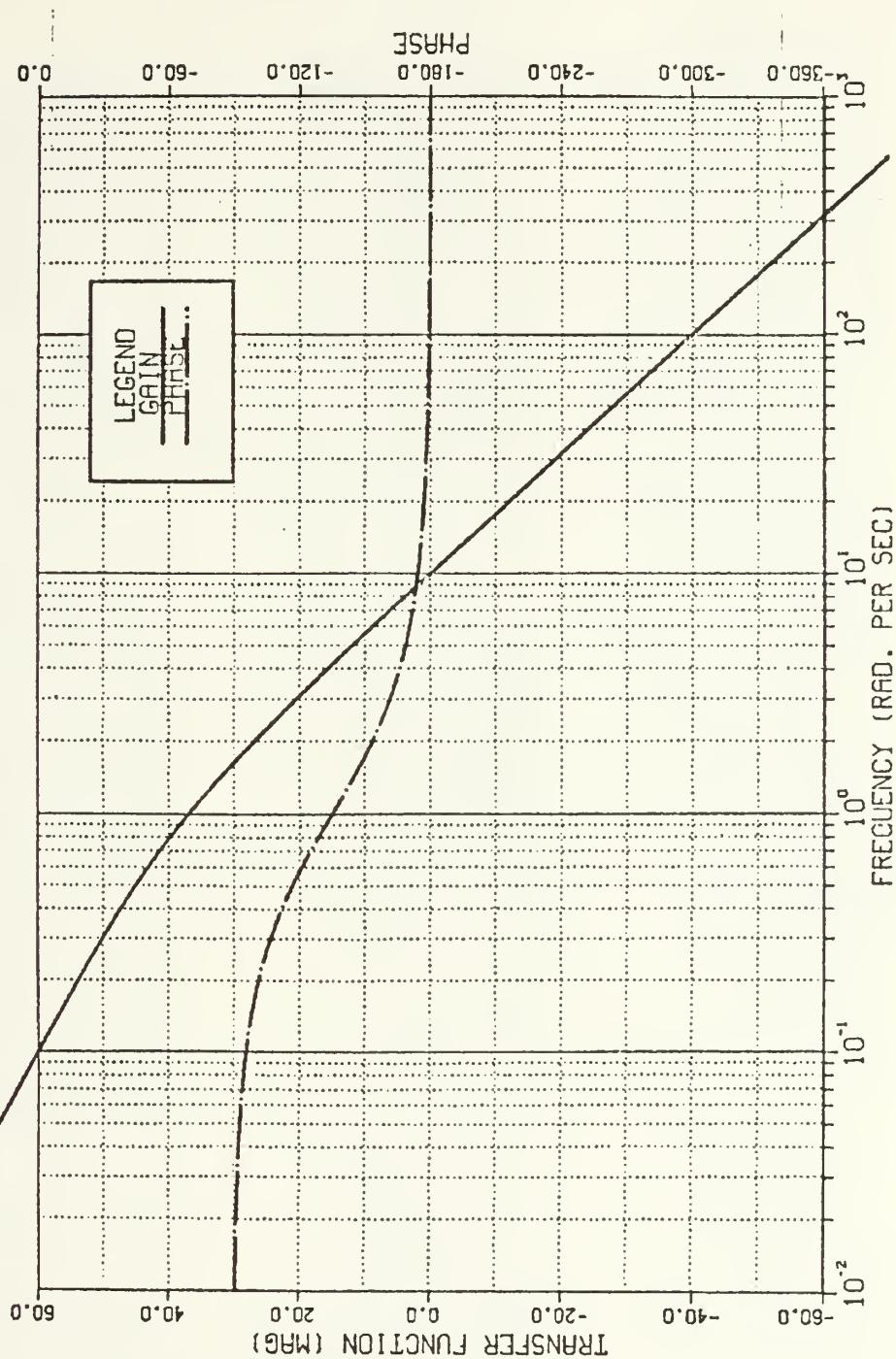


Figure 6. Uncompensated Bode Plot of Example 4.3

EXAMPLE 4.3
VELOCITY FEEDBACK

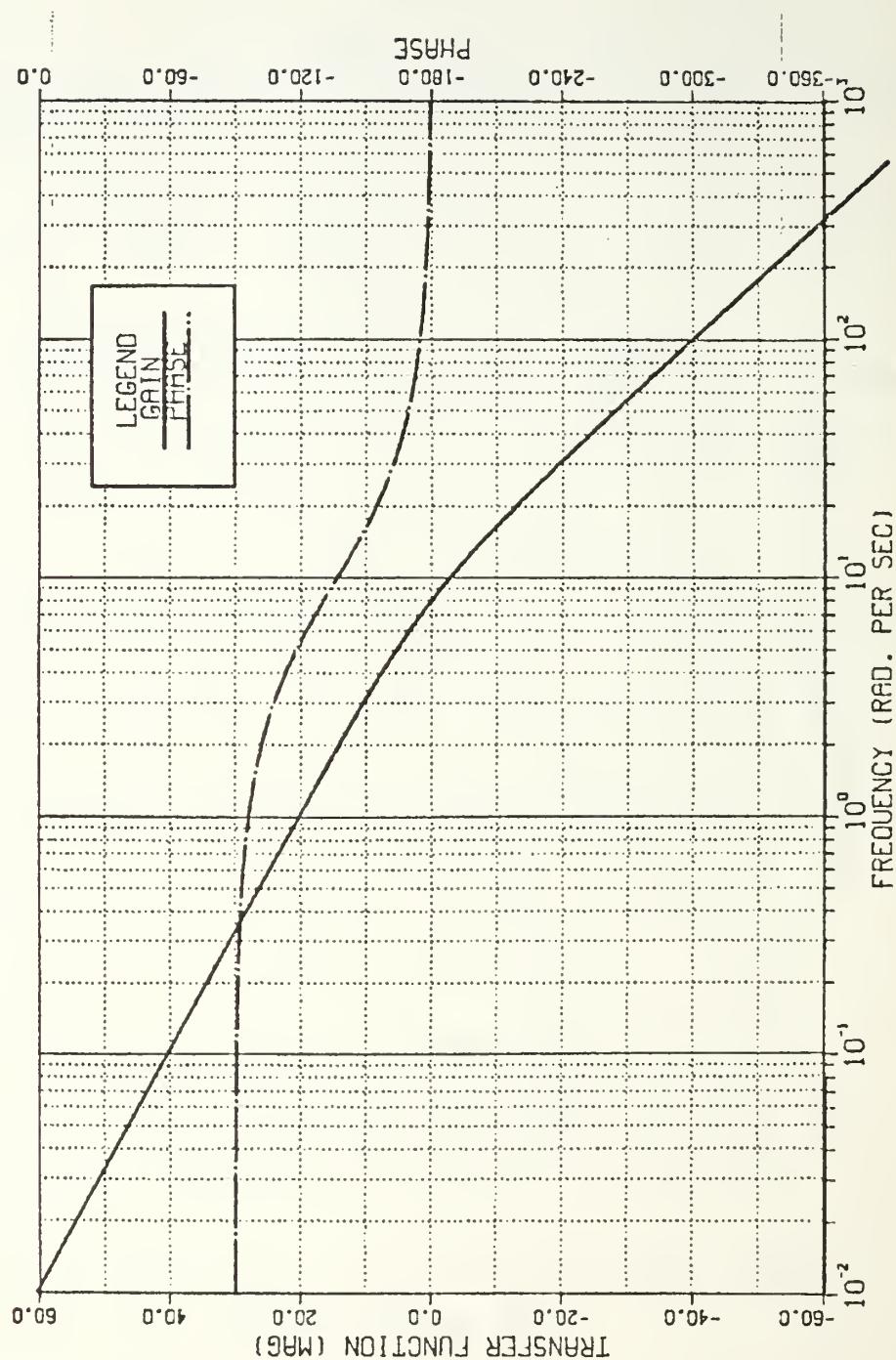


Figure 7. Velocity Feedback Used in Example 4.3

Table 3. Tabular Output of Example 4.3

FREQ	MAGNITUDE	PHASE
0.100000E+01	0.606303E+02	-0.900604E+02
0.113646E+01	0.595494E+02	-0.900688E+02
0.129155E+01	0.584081E+02	-0.900784E+02
0.146780E+01	0.572970E+02	-0.900892E+02
0.166810E+01	0.561859E+02	-0.901016E+02
0.189573E+01	0.550747E+02	-0.901156E+02
0.215443E+01	0.539636E+02	-0.901310E+02
0.244843E+01	0.528525E+02	-0.901497E+02
0.278250E+01	0.517414E+02	-0.901703E+02
0.316227E+01	0.506303E+02	-0.901936E+02
0.359381E+01	0.495192E+02	-0.902202E+02
0.408423E+01	0.484080E+02	-0.902504E+02
0.464159E+01	0.472969E+02	-0.902848E+02
0.527499E+01	0.461858E+02	-0.903238E+02
0.599483E+01	0.450746E+02	-0.903682E+02
0.681291E+01	0.439635E+02	-0.904185E+02
0.774263E+01	0.428523E+02	-0.904758E+02
0.879921E+01	0.417411E+02	-0.905409E+02
0.999998E+01	0.406298E+02	-0.906149E+02
0.113646E+00	0.395186E+02	-0.906989E+02
0.129155E+00	0.384073E+02	-0.907945E+02
0.146780E+00	0.372959E+02	-0.909030E+02
0.166810E+00	0.361845E+02	-0.910204E+02
0.189573E+00	0.350730E+02	-0.911666E+02
0.215443E+00	0.339613E+02	-0.913259E+02
0.244843E+00	0.328495E+02	-0.915069E+02
0.278255E+00	0.317376E+02	-0.917120E+02
0.316227E+00	0.306253E+02	-0.919465E+02
0.359381E+00	0.295127E+02	-0.922118E+02
0.408423E+00	0.283997E+02	-0.925134E+02
0.464157E+00	0.272862E+02	-0.928500E+02
0.527498E+00	0.261720E+02	-0.932451E+02
0.599483E+00	0.250568E+02	-0.936870E+02
0.681291E+00	0.239404E+02	-0.941880E+02
0.774262E+00	0.228226E+02	-0.947579E+02
0.879919E+00	0.217028E+02	-0.954037E+02
0.999996E+00	0.205804E+02	-0.961360E+02
0.113646E+01	0.194549E+02	-0.969657E+02
0.129155E+01	0.183252E+02	-0.979052E+02
0.146779E+01	0.171902E+02	-0.989075E+02
0.166809E+01	0.160484E+02	-0.100167E+03
0.189573E+01	0.148980E+02	-0.104520E+03
0.215443E+01	0.137367E+02	-0.105042E+03
0.244843E+01	0.125615E+02	-0.104748E+03
0.278255E+01	0.113691E+02	-0.106650E+03
0.316227E+01	0.101552E+02	-0.108778E+03
0.359381E+01	0.891480E+01	-0.111147E+03
0.408423E+01	0.764222E+01	-0.113708E+03
0.464157E+01	0.633108E+01	-0.116522E+03
0.527498E+01	0.497453E+01	-0.119560E+03
0.599482E+01	0.356567E+01	-0.128044E+03
0.681290E+01	0.209793E+01	-0.132424E+03
0.774261E+01	0.565706E+00	-0.129777E+03
0.879919E+01	-0.103506E+01	-0.133413E+03
0.999996E+01	-0.270049E+01	-0.137075E+03
0.113646E+02	-0.444846E+01	-0.140704E+03
0.129155E+02	-0.625853E+01	-0.144242E+03
0.146779E+02	-0.813240E+01	-0.147639E+03
0.166809E+02	-0.100643E+02	-0.150857E+03
0.189573E+02	-0.120476E+02	-0.153860E+03

Table 3. (Contd.)

0.215443E+02	-0.140753E+02	-0.156650E+03
0.244843E+C2	-0.161408E+02	-0.159199E+03
0.278255E+C2	-0.182376E+02	-0.161517E+03
0.316226E+C2	-0.203602E+02	-0.163609E+03
0.359380E+C2	-0.225037E+02	-0.165489E+03
0.408423E+C2	-0.246639E+02	-0.167170E+03
0.464157E+C2	-0.268375E+02	-0.168668E+03
0.527497E+C2	-0.290217E+02	-0.169999E+03
0.599482E+02	-0.312143E+02	-0.171179E+03
0.681290E+C2	-0.334134E+02	-0.172224E+03
0.774261E+C2	-0.356177E+02	-0.173448E+03
0.879919E+02	-0.378259E+02	-0.173964E+03
0.999955E+C2	-0.400373E+02	-0.174084E+03
0.113646E+03	-0.422511E+02	-0.175319E+03
0.129154E+C3	-0.444068E+02	-0.175079E+03
0.140779E+C3	-0.466840E+02	-0.176374E+03
0.166809E+03	-0.489023E+02	-0.176806E+03
0.189573E+C3	-0.511215E+02	-0.177189E+03
0.215443E+C3	-0.533413E+02	-0.177520E+03
0.244843E+03	-0.555617E+02	-0.177822E+03
0.278255E+C3	-0.577825E+02	-0.178083E+03
0.310426E+C3	-0.600037E+02	-0.178313E+03
0.359379E+C3	-0.622250E+02	-0.178515E+03
0.408422E+C3	-0.644466E+02	-0.178093E+03
0.464157E+03	-0.666683E+02	-0.178850E+03
0.527497E+C3	-0.688902E+02	-0.178988E+03
0.599481E+C3	-0.711121E+02	-0.179109E+03
0.681290E+03	-0.733341E+02	-0.179215E+03
0.774260E+C3	-0.755564E+02	-0.179309E+03
0.879918E+C3	-0.777782E+02	-0.179394E+03
0.999957E+03	-0.800003E+02	-0.179465E+03

EXAMPLE 4.3

CLOSED LOOP RESPONSE

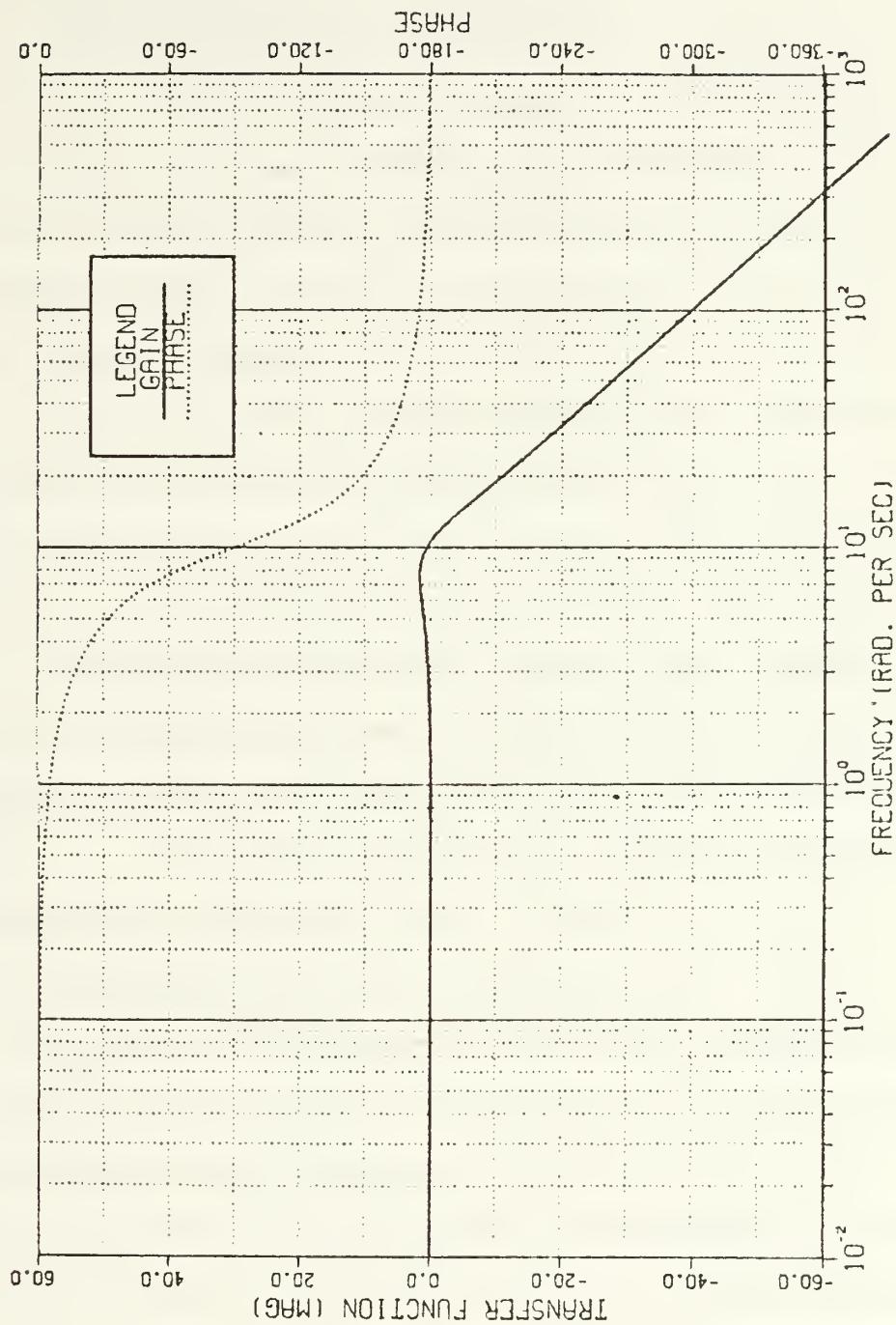


Figure 8. Closed Loop Response of Example 4.3

V. CONCLUSION AND RECOMMENDATIONS

A. CONCLUSION

The objective of this thesis was to develop an interactive user oriented computer program which would aid in solving control engineering problems using the Bode method of design. The presented program proves that frequency domain design of control systems using the digital computer as an aid is not only feasible but highly desirable. The results obtained are readily interpretable and provide good and meaningful insight into the problem.

The results obtained during the investigation of the program performance show that a complicated but well formulated problem can be solved with ease, and the solution is obtained with speed, accuracy and precision.

The entire program is less than 1000 lines, with a total of 9 subroutines. Every effort has been made to keep the program simple yet unambiguous, so that the user has to invest very little time learning how to use it. Effort has also been made to minimize the use of the computer CPU time. However, expenditure of CPU time is to a large measure dependent upon:

- (1) the order of the system.
- (2) the number of iterations used in reaching a solution.

(3) the type and order of the compensator(s) used.

B. RECOMMENDATIONS

The program as presented in this thesis seems to be able to adequately satisfy the usual needs in a control system design problem. A number of useful extensions to the work developed in this thesis can be carried out. These are briefly discussed.

1. Curve Fitting

Although not specifically worked on in this thesis, the program can be used quite effectively for curve fitting purposes. This was demonstrated in the initial stages of the development of this program. The procedure is, by its very nature, iterative and therefore time consuming and cumbersome. However, the entire algorithm can be automated using a minimization subroutine, with the program outputting a polynomial to fit a given curve over a specified range of the independent variable.

2. Computer Selection of Compensators

A suitable minimization routine such as Box PLX can be incorporated into the program which could select the best possible location of poles and zeroes to meet given performance specifications. This would automate the entire Bode design procedure, the user then having the option of only specifying the type of compensation, i.e., cascade or feedback. It may however be pointed out that minimization

routines by the very nature of their operation are very time consuming and wasteful of CPU resources.

3. Root Locus

Most of the subroutines developed in this thesis are very general in nature and can be adapted quite easily to develop a similar interactive program for Root Locus plots.

4. Integrated Control System Design

No meaningful design of control systems is complete without finally analyzing its time domain performance. It is therefore considered highly desirable to incorporate into this program, an interactive Root Locus design procedure and then a time domain analysis of the compensated system. The entire package would then be an excellent teaching aid for control system design.

APPENDIX PROGRAM LISTING

308

GO TO 3C3
CONTINUE
CALL FR7CMS(• CLRSCRN•)
RETURN

```

C***** WRITE FORMAT STATEMENTS *****
C
C351  FORMAT (//,7X, *ENTER ORDER OF NUMERATOR POLYNOMIAL AS A 1*, )
C      *   FORMAT (//,7X, *ENTER ORDER OF INTEGER*)
C352  *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C      *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C353  *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C      *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C354  *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C      *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C355  *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C      *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C356  *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C      *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C360  *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C      *   FORMAT (//,7X, *ENTER COEFICIENT OF NUMERATOR POLYNOMIAL IS 0,1,4,X, )
C***** READ FORMAT STATEMENTS *****
C
C376  FORMAT (1I1)
C377  FORMAT (A1)
C378  FORMAT (F14.4)
C379  FORMAT (A1)
C
C***** END *****

```

SUBROUTINE DENUM (DA)

```

C   **** SUBROUTINE TO INPUT THE DENOMINATOR *
C   * CF THE PLANT TRANSFER FUNCTION *
C   **** **** **** **** **** **** **** **** ****
C   ** VARIABLE DECLARATIONS ***
C   INTEGER ANSWER,YES
C   REAL DA
C   DIMENSION DA(10)
C   DATA YES/'Y./
C
C   DO 401 I=1,10
C   DA(I)=0.0
C   CONTINUE
C   CALL FRICMS('CLRSRNM')
C   WRITE(6,451)
C   READ(5,476)N
C   WRITE(6,452)N
C   READ(5,477)ANSWER
C   IF (ANSWER .EQ. YES) GO TO 402
C   GO TO 401
C   CONTINUE
C   N=N+1
C   CONTINUE
C
C   CALL FRICMS('CLRSRNM')
C   WRITE(6,460)
C   DO 406 I=1,N
C   J=I-1
C   WRITE(6,453)J
C   READ(5,478,END=405) DA(I)
C   GO TO 406
C   REWIND 5
C   CALL FRICMS('CLRSRNM')
C   WRITE(5,456)
C   DO TO 404
C   CONTINUE
C   CALL FRICMS('CLRSRNM')
C   DU 407 I=1,N
C   J=N-1
C   K=J+1
C   WRITE(6,454) J,DA(K)
C   CONTINUE
C   WRITE(6,455)
C   READ(5,479)ANSWER
C   IF (ANSWER .EQ. YES) GO TO 408

```

```

60 TO 4C3
CONTINUE
CALL FR7CMS('CLRSRN')
RETURN

C***** WRITE FORMAT STATEMENTS *****
C
451  FORMAT(1/1.7X,'ENTER ORDER OF DENOMINATOR POLYNOMIAL AS A 1.',*
        *      '1 DIGIT NUMBER')
452  FORMAT(1/1.7X,'ORDER OF DENOMINATOR POLYNOMIAL IS ',11,4X,*
        *      'CORRECT? (Y/N),')
453  FORMAT(1/1.7X,'ENTER COEFFICIENT OF S***(1,12,0)')*
454  FORMAT(1/1.7X,'COEFFICIENT OF 12',*14.0)
455  FORMAT(1/1.7X,'ARE THE ABOVE COEFFICIENTS CORRECT? (Y/N)')*
456  FORMAT(1/1.7X,'YOU HAVE PRESSED "ENTER" WITHOUT ENTERING ANY',*
        *      'NUMBER. TRY AGAIN.')
460  FORMAT(1/1.7X,'ALL DENOMINATOR COEFFICIENTS MUST BE ENTERED',*
        *      'IN DECIMAL FORMAT.')
C***** READ FORMAT STATEMENTS *****
C
470  FORMAT(11)
477  FORMAT(11)
478  FORMAT(F14.4)
479  FORMAT(11)
C
END

```


SUBROUTINE SECAS(CN)

```

C **** SUBROUTINE TO INPUT THE NUMERATOR *
C * UF THE SECOND ORDER COMPENSATOR *
C **** **** **** **** **** **** **** ****
C ** VARIABLE DECLARATIONS ***
C ** INTEGER ANSWER, YES
REAL CN
DIMENSION CN(3)
DATA YES/.Y./

C CALL FRICMS('CLRSRN')
CONTINUE
301 WRITE(6,351)
DO 306 I=1,2
J=J-1
CONTINUE
WRITE(6,353) J
READ(5,378,END=305) CN(1)
GOTO 306
REWIND 5
CALL FRICMS('CLRSRN')
WRITE(5,350)
DO 304
CONTINUE
CALL FRICMS('CLRSRN')
DO 307 I=1,3
J=J-1
K=J+1
WRITE(6,354) J,CN(K)
CONTINUE
WRITE(6,355)
READ(5,379) ANSWER
IF(ANSWER.EQ.YES) GO TO 308
DO 301
CONTINUE
CALL FRICMS('CLRSRN')
RETURN
307
308
C **** **** **** **** **** **** **** ****
C 351 FORMAT(17X,'COEFFICIENTS OF NUMERATOR OF SECOND '
C * 'ORDER CASCADÉ COMPENSATOR',7X,'ENTER ALL ',I,
C * 'COEFFICIENTS IN DECIMAL FORMAT')

```

```

353 FORMAT(//,7X,"ENTER COEFFICIENT OF S**12.",E4.0)
354 FORMAT(//,7X,"COEFFICIENT OF S**12.",E4.0)
355 FORMAT(//,7X,"ARE THE ABOVE COEFFICIENTS CORRECT?",Y/N)
356 FORMAT(//,7X,"YOU HAVE PRESSED 'ENTER' WITHOUT ENTERING ANY.",*)
*                                **** READ FORMAT STATEMENTS ****
C*****FORMAT(F14.0)      ****
C*****FORMAT(A1)          ****
378 *****FORMAT(F14.0)
379 *****FORMAT(A1)
C

```

SUBROUTINE SECASD(CC)

CALL FRICMS (• CLRSCRN •)

401
CONTINUE
WRITE(6,451)
DO 406 I=1,3
406

404 $\sum_{i=1}^{10} \text{WRITE} \left(\frac{6,453}{5,478}, \text{END} = 405 \right) \text{CD}(1)$

405 GO TO 406
RE WIND⁵
CALL FRICMS. (• CLRSCRN•)

```

406
      WRITE(5,456)
      GO TO 4C4
      CONTINUE
      CALL FRICMS("CLRS CRN")
      DO 407 I=1,3

```

```
2.2  
J = J-1  
K = J+1  
WRITE(6,454) J,CD(K)
```

407
CCNTLINE
WRITE(6,455)
READ(5,479)ANSWER
11F(ANSWER,0,YES)
GO TO 408

```
455      FORMAT(//,7X,*)  ARE THE ABOVE COEFFICIENTS CORRECT? (Y/N) *)
456      FORMAT(//,7X,*)  YOU HAVE PRESSED "ENTER" WITHOUT ENTERING ANY*,,
*      NUMBER.,/,7X,*, TRY AGAIN. *)
C***** READ  FORMAT  STATEMENTS  ****
C***** FORMAT(A1)  ****
478      FORMAT(F14.0)
479      FORMAT(A1)
C      END
```


SUBROUTINE `FETCH (FENUM)`

SUBROUTINE DECADE(DEC)

```

C   **** SUBROUTINE TO INPUT THE NUMBER OF
C   * DECADES OF FREQUENCY TO BE SPANNED. *
C   * ***** VARIABLE DECLARATIONS *****
C   * INTEGER DEC, ANSWER, YES
C   DATA YES/1/
```

101

```

CONTINUE
WRITE(6,151)
READ(5,176,END=102)DEC
CALL FRICMS(0,CLRS CRN)
GU TO 153
REWIND 5
CALL FRICMS(0,CLRS CRN)
GU TO 152
WRITE(6,152)
GU TO 151
CONTINUE
WRITE(6,153)DEC
READ(5,177)ANSWER
IF (ANSWER.EQ.YES) GO TO 104
GO TO 151
CONTINUE
RETURN
```

```

C***** WRITE FORMAT STATEMENTS *****
151 * FORMAT(0,1,7X) ENTER AS A SINGLE DIGIT INTEGER NUMBER.
* FORMAT(0,1,7X) FREQUENCY TO BE SPANNED.
* FORMAT(1,1,7X) MAXIMUM : MINIMUM : 1.
* FORMAT(1,1,7X) YOU HAVE PRESSED "ENTER" WITHOUT ENTERING ANY .
153 * FORMAT(1,1,7X) TRY AGAIN.
* FORMAT(5,1,7X) DECADES OF FREQUENCY WILL BE SPANNED.
C***** READ FORMAT STATEMENTS *****
176 FORMAT(1,1)
177 FORMAT(1,1)
C   END
C
```

```

DEC00010
DEC00020
DEC00030
DEC00040
DEC00050
DEC00060
DEC00070
DEC00080
DEC00090
DEC00100
DEC00110
DEC00120
DEC00130
DEC00140
DEC00150
DEC00160
DEC00170
DEC00180
DEC00190
DEC00200
DEC00210
DEC00220
DEC00230
DEC00240
DEC00250
DEC00260
DEC00270
DEC00280
DEC00290
DEC00300
DEC00310
DEC00320
DEC00330
DEC00340
DEC00350
DEC00360
DEC00370
DEC00380
DEC00390
DEC00400
DEC00410
DEC00420
DEC00430
DEC00440
DEC00450
DEC00460
```

```

SUBROUTINE TITLES( TTL1, MSS1 )
C
C***SUBROUTINE TO INPUT TWO LINES
C   AS PLOTLINES FOR THE BUDGET PLOTS
C***DEclaration of Variables
C
C      INTEGER TTL1, MSS1
C      DIMENSION TTL1(5), MSS1(5)
C      WRITE(6,51)
C      READ(5,676) TTL1(1), TTL1(2), TTL1(3), TTL1(4), TTL1(5)
C      WRITE(6,653)
C      READ(2,676) MSS1(1), MSS1(2), MSS1(3), MSS1(4), MSS1(5)
C      RETURN
C
C***      WRITE FORMAT STATEMENTS
C
651  FORMAT(//7X,* YOU MAY WRITE TWO LINES OF TEXT AS HEADING ON THE *,
C      * BCODE FLOT; //7X,* ENTER FIRST LINE (MAXIMUM 20 CHARACTERS),
C      * FORMAT(7X,ENTER SECOND LINE OF TEXT (MAXIMUM 20 CHARACTERS).)
C
C***      READ FORMAT STATEMENT
C
676  FORMAT(4,A4,A4,A4,A4)
C      END

```



```

CALL SECASE(CN1)
CALL SECASE(CD1)
CONTINUE
WRITE(6,1000)
READ(5,107)ANSWER.EQ.YES.GG TGOALS
IF(.NOT.ANSWER.EQ.YES)GO TO 1015
CALL FEELER(FK,FN,FL,FF)
CONTINUE
CALL INFECT(NUML)
CALL FECACE(DECS)
CALL TFILE(TITLE,MESS)
CONTINUE
ADECS = FLOAT(DECS)
WRITE(5,107C)
READ(5,107)ANS2
DO 10 1 = 1,71
LOGH(1) = (I-1)/270.*ADECS
FREQ(1) = (10.0**LOGH(1))*10.**(NUM)
S = CNFLX(2,FREQ(1))
C***** UNCOMPENSATED SYSTEM : NUMERATOR *****
C
N = A(1)*(S**0) + A(2)*(S**1) + A(3)*(S**2) + A(4)*(S**3)
* + A(5)*(S**4) + A(6)*(S**5) + A(7)*(S**6) + A(8)*(S**7)
* + A(9)*(S**8) + A(10)*(S**9)
C***** UNCOMPENSATED SYSTEM : DENOMINATOR *****
C
D = B(1)*(S**0) + B(2)*(S**1) + B(3)*(S**2) + B(4)*(S**3)
* + B(5)*(S**4) + B(6)*(S**5) + B(7)*(S**6)
* + B(8)*(S**7) + B(9)*(S**8) + B(10)*(S**9)
hPLANT = N/D
C***** FIRST ORDER CASCADE FILTERS *****
C
NCA5 = ((S/CZ(4))+1.)*( (S/CZ(5))+1.)*( (S/CZ(6))+1.)*
* ((S/CZ(7))+1.)*((S/CZ(8))+1.)*((S/CZ(9))+1.)*
DCAS = ((S/CP(4))+1.)*( (S/CP(5))+1.)*( (S/CP(6))+1.)*
* ((S/CP(7))+1.)*((S/CP(8))+1.)*((S/CP(9))+1.)*
HCAS = NCAS/DCAS
C***** SECOND ORDER CASCADE FILTERS *****
C
NCAS2 = (CN1(2)*(S**2)+CN1(1)*(S**1)+CN1(1))
* (CN2(3)*(S**2)+CN2(2)*(S**1)+CN2(1))
DCAS2 = (CL1(3)*(S**2)+CL1(2)*(S**1)+CL1(1))
* (CL2(3)*(S**2)+CL2(2)*(S**1)+CL2(1))

```

SEC II - INCASSO

NATIONAL COMPENSATION SURVEY

IF (.NOT. ANSI .EQ. YES) DO 1014

900

LIST OF REFERENCES

1. Gianniotis, Demetrios D., Interactive Control System Optimization and Simulation, Thesis Dissertation, Naval Postgraduate School, October 1982.
2. Thaler, G.J., Design of Feedback Systems, Dowden Hutchinson and Ross, Inc., 1973
3. Ward, J.R., and Strum, R.D., State Variable Analysis, Naval Postgraduate School, Monterey, California, 1975.
4. Luenberger, D.G., Introduction to Linear and Nonlinear Programming, Addison-Wesley Publishing Company, Inc. 1973.
5. Kuo, Benjamin C., Automatic Control Systems, Prentice-Hall, Inc., 1982.
6. Thaler, G.J., Automatic Control Systems, Naval Post-graduate School, 1984.
7. Bazarra, M.S., Nonlinear Programming, Theory and Algorithms, John Wiley and Sons, Inc., 1979
8. Box, M.J., "A New Method of Constraint Optimization and a Comparison with Other Methods," Computer Journal, pp. 45-52, 8 April 1965.
9. Schaum's Outline Series, Programming With Fortran, McGraw-Hill Book Company, 1978.
10. W.R. Church Computer Center, Technical Note, "User's Guide to VM/CMS at NPS," April 1981.
11. W.R. Church Computer Center, Technical Note, "Using Disspla at NPS," June 1984.
12. Integrated Software Systems Corporation, "Disspla Users' Manual," October 1981.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Library, Code 0142 Naval Postgraduate School Monterey, California 93943	2 .
2. Professor George J. Thaler, Code 62TR Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, California 93943	5
3. Professor Alex Gerba, Jr., Code 62GZ Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, California 93943	1
4. Department Chairman, Code 62RR Department of Electrical and Computer Engineering Naval Postgraduate School Monterey, California 93943	1
5. Naval Secretary Naval Headquarters Islamabad Pakistan	1
6. Directorate of Naval Training Naval Headquarters Islamabad Pakistan	1
7. Directorate of Naval Weapons and Equipment Naval Headquarters Islamabad Pakistan.	1
8. Commander Karachi 9 Liaquat Barracks Karachi Pakistan	1

9.	Commanding Officer Pakistan Naval Engineering College Habib Ibrahim Rahimtoola Road Karachi Pakistan	1
10.	LCDR Habib Ismail, P.N. Pakistan Naval Engineering College PNS Jauhar Habib Ibrahim Rahimtoola Road Karachi Pakistan	5
11.	LCDR M. Tariq, P.N. Pakistan Naval Engineering College PNS Jauhar Habib Ibrahim Rahimtoola Road Karachi Pakistan	1
12.	Tayfun Tansan Goztepe Istasyon Cad. Np. 31/13 Istanbul Turkey	1
13.	LT Kyritsis-Spromilios Pericles, H.N. Sarantaporou 125 Papagou Athens Greece	1
14.	LT Horianopoulos Emmanuel, H.N. Travlantoni 39 Patisia Athens Greece	1
15.	Defense Technical Information Center Cameron Station Alexandria, Virginia 22314	2

21843

Thesis
I727 Ismail
c.1 Interactive computer
program for the analy-
sis and design of
linear time invariant
systems.

21843

Thesis
I727 Ismail
c.1 Interactive computer
program for the analy-
sis and design of
linear time invariant
systems.

thesis1727

Interactive computer program for the ana



3 2768 001 02574 5

DUDLEY KNOX LIBRARY